

Wavelength-dependent multifunctional metalens devices via genetic optimization

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Abstract: Metalenses with non-trivial performance, abundant applications, and tremendous potential, have emerged as a flat optical element or configuration in recent years. The increasing concerns about how to integrate more functions into a single metalens have become a hot topic. Here, based on a genetic algorithm, we demonstrate several metalenses with more than two optical functions depending on the wavelength of light. We first design three arbitrary chromatic dispersive metalenses, whose focal planes can be determined at will at different wavelengths. Then, a metalens-based color router is presented, which is able to guide and focus the light with four wavelengths to different positions. Furthermore, we exhibit a tri-functional structured light generator to produce focused beam, focused orbital angular momentum beam, and the Bessel beam at three wavelengths, respectively. Our results may have potential applications in dispersion manipulation, optical micro-manipulation, and subwavelength resolution spectral imaging.

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1. Introduction

Traditional optical elements or configurations are gradually replaced by planar diffractive elements (PDEs) due to their bulky size and complex system. As one of the promising PDEs, metasurface, consisting of the array of subwavelength nano-units, plays a crucial role during the last decade, especially metalenses, which can not only realize diffraction-limit focusing and full-color imaging but also attribute to their compact volumes [1–5]. Fundamental strategies of metalens design mainly classify into three types. Among them, most of works are based on the geometrical (Pancharatnam-Berry) phase for circularly polarization operation, some are dependent on propagation phase in dielectric waveguide segments and others are follows by multiple resonance on the unit cell [6]. Meanwhile, increasing metasurface devices arise in the field of quantum source [7,8], nonlinear optics [9,10] and other specific applications like spectroscopies [11], endoscopes [12] and meta-fibers [13].

The other major superiority of metalenses is their multifunctionality. Precisely manipulating multidimensional optical parameters of light field can achieve different phase or amplitude distributions. For example, orthogonal polarizations are important parameters of light that can be completely implemented to realize absolutely independent phase profiles [13–19]. By designing the metalens with different incident angles, various optical responses can also be obtained in the reflection plane [20]. Therefore, how to further add more functionalities in a single-layer metasurface has a strong appeal to the researchers. Theoretically, wavelengths have unlimited capability, which has been demonstrated on a reflective metasurfaces in the previous work [21], but fail to perform the transmissive functionalities owing to its reflection. Besides, the metalens reported by another work has achieved only two kinds of light-field manipulation within a certain bandwidth and cannot be polarization-insensitive [22], which greatly impacts the multiplexing of metalens. Here, we design the multifunctional metalenses to realize two more

functionalities at corresponding wavelengths through arranging three kinds of centrosymmetric nanopillars with polarization-independent features by genetic algorithm in the near-infrared regime. Through this scheme, arbitrary focal planes at different wavelengths incidence can be achieved and two meta-devices named color router and tri-functional structured light generator are revealed, respectively. This work is a further extension of dispersion-engineering and we envision it to occupy a position in multifunctional optical platforms.

2. Principle of the metalens design

Our design principle is mainly implemented by the appropriate arrangement of three centrosymmetric dielectric nanopillars, whose phase shifts depends on the propagation phase with polarization-independent property, therefore, a phase library of nanopillars to realize the required phase shifts should be built. In this work, we design three basic structures labeled as A, B and C to cover $0-2\pi$ in phase space, which is shown in Fig. 1(a). These centrosymmetric nanopillars composed of silicon (Si) on a fused silica (SiO_2) substrate can be considered as truncated waveguides [23] because of the high-index contrast between the nanopillar ($n_{\text{Si}}=3.48$) and air ($n_{\text{air}}=1$). Finite-difference time domain (FDTD) simulations are performed to acquire phase shifts of nanopillars for 5 nm increment of each geometric parameter by using the commercial software package “FDTD Solutions” (Lumerical Inc.). Periodic boundary conditions are applied along the x and y axes, and the perfectly matched layers (PMLs) are applied to the z direction. The sweeping scope of lengths (L) and widths (W) of the nanopillars covers 50 nm to 600 nm with fixed Height (H) $H = 1 \mu\text{m}$, and the properly arranged array of nanopillars have a lattice constant of $P_x = P_y = 600 \text{ nm}$. The results of phase shifts of all the nanopillars for four wavelengths spread out on the entire $2\pi \times 2\pi$ square, which are illustrated in Fig. 1(b).

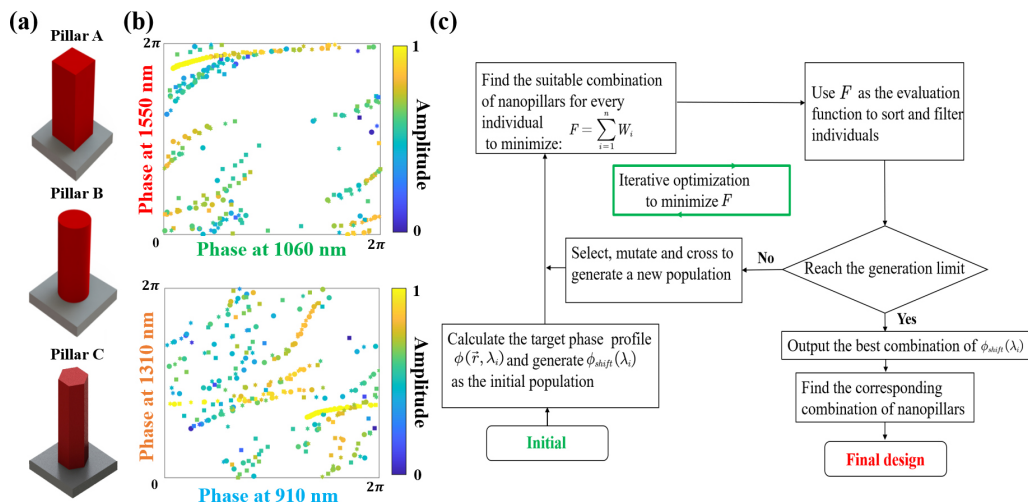


Fig. 1. (a). Typical nanopillars of our design. (b). Phase library of nanopillars for four wavelengths response in the $2\pi \times 2\pi$ phase space, square, circular and star points corresponds to the designed pillar A, B and C (phase shifter). Color map represents the amplitudes of typical pillars. (c). Flow chart of genetic algorithm applied in design principle.

The independent phase shifts for each wavelength provide possibility to realize multifunctional devices. However, it can be seen from Fig. 1(b) that the phase shifts cannot exactly cover every corner of the phase space, and it still requires larger phase space to successfully realize the required metalens. Therefore, the optimization of genetic algorithm has been chosen for the suitable arrangement of nanopillars, and $\Phi_{\text{shift}}(\lambda_i)$ is introduced as a constant value to amend and

optimize the phase profile, which is unable to impact the objective functions for it only changes the absolute phase of every λ_i instead of relative phase. The $\varphi_i(x, y, \lambda_i)$ represents the target phase at the coordinate (x, y) for wavelength λ_i , and $\varphi_{\text{real}}(x, y, \lambda_i)$ is the phase saved in the library of the chosen pillar at the specific site (x, y) . In order to get the optimized $\Phi_{\text{shift}}(\lambda_i)$ for every λ_i [24], we choose to adopt the genetic algorithm. We first define the residue function R_i , which is used to measure the matching degree between the real phase $\varphi_{\text{real}}(x, y, \lambda_i)$ and the adjusted target phase profile $\varphi_i(x, y, \lambda_i) + \Phi_{\text{shift}}(\lambda_i)$. R_i is defined as:

$$R_i = \sum_{j=1}^N |e^{i\varphi_{\text{real}}(\vec{x}, \vec{y}, \lambda_i)} - e^{i[\varphi_i(\vec{x}, \vec{y}, \lambda_i) + \Phi_{\text{shift}}(\lambda_i)]}| \quad (1)$$

where N is the number of nanopillars placed in the metalenses. Considering that different functions have different tolerances to residuals, we introduce weighted residue function W_i as:

$$W_i = \beta_i R_i = \beta_i \sum_{j=1}^N |e^{i\varphi_{\text{real}}(\vec{x}, \vec{y}, \lambda_i)} - e^{i[\varphi_i(\vec{x}, \vec{y}, \lambda_i) + \Phi_{\text{shift}}(\lambda_i)]}| \quad (2)$$

where β_i represents a parameter weighing the tolerance to residues requiring multiple adjustments based on simulation results. Clearly, the high β_i means the low tolerance to residues for function i . The genetic algorithm to determine $\Phi_{\text{shift}}(\lambda_i)$ is applied for every λ_i . Here, the fitness function F can be defined as:

$$F = \sum_{i=1}^n W_i = \sum_{i=1}^n \beta_i \sum_{j=1}^N |e^{i\varphi_{\text{real}}(\vec{x}, \vec{y}, \lambda_i)} - e^{i[\varphi_i(\vec{x}, \vec{y}, \lambda_i) + \Phi_{\text{shift}}(\lambda_i)]}| \quad (3)$$

where n denotes the number of working wavelengths. Using the $\Phi_{\text{shift}}(\lambda_i)$ produced by the genetic algorithm, the best arrangement of nanopillars to minimize the fitness function F can be obtained. The flow chart of optimization based on genetic algorithm is shown in Fig. 1(c). Subsequently, the simulation of objective metalenses has been numerically demonstrated by adjusting β_i according to the results, until all target functionalities can be simultaneously achieved.

3. Result and discussion

3.1. Chromatic dispersion manipulation

The left parts of Fig. 2(a)-(c) schematically show the three metalenses ($R=8 \mu\text{m}$) that arbitrarily control chromatic dispersion at four wavelengths in the near-infrared regime (910 nm, 1060 nm, 1310 nm, 1550 nm). As a verification of our design scheme, metalens 1 exhibits achromatic focusing at $f=15 \mu\text{m}$ for all four wavelengths, and metalens 2 displays achromatic capabilities with separate focal lengths for 1550 nm and 1310 nm at $f_1=15 \mu\text{m}$, 1060 nm and 910 nm at $f_2=9 \mu\text{m}$, respectively. While metalens 3 employs another situation that 1550 nm and 1060 nm focus at $f_1=15 \mu\text{m}$ and 1310 nm and 910 nm focus at $f_1=9 \mu\text{m}$. The corresponding phase profiles of our design with double focal lengths characteristics satisfy the following functions:

$$\varphi_1(x, y, \lambda_i) = -\frac{2\pi}{\lambda_i}(\sqrt{x^2 + y^2 + f_1^2} - f_1) \quad (4)$$

$$\varphi_2(x, y, \lambda_i) = -\frac{2\pi}{\lambda_i}(\sqrt{x^2 + y^2 + f_2^2} - f_2) \quad (5)$$

where λ_i is the design wavelength, (x, y) represents the position of each nanopillar on the metalenses, f_1 and f_2 are the focal lengths. Note that when $f_1=f_2=15 \mu\text{m}$, the achromatic metalens can be satisfied.

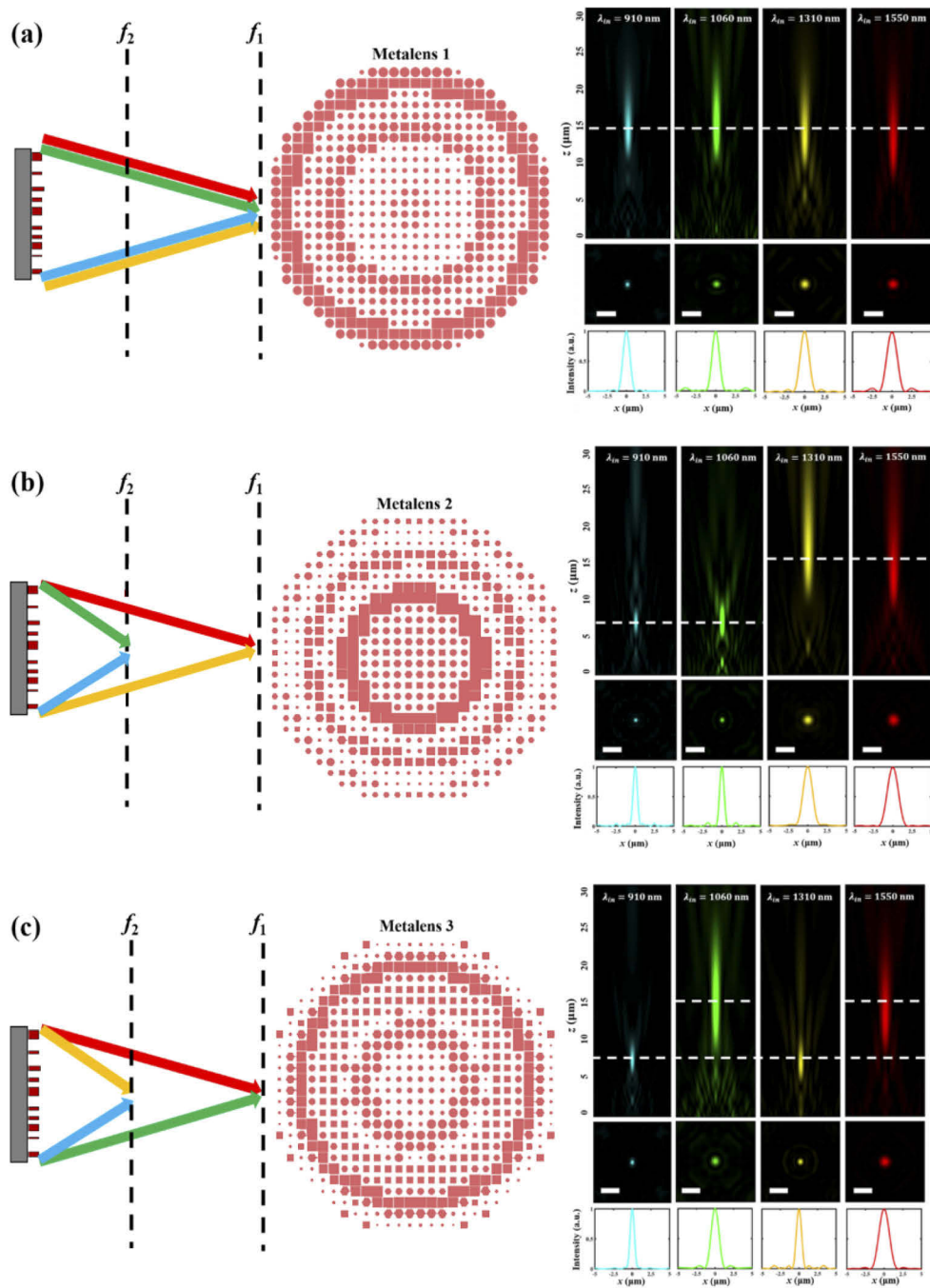


Fig. 2. Schematic diagram of chromatic dispersion manipulation based on metalenses (left inset in (a), (b) and (c)), configuration of metalenses (middle inset in (a), (b) and (c)) and simulated longitudinal intensity distributions, transverse intensity distributions (scale bar: $2\mu\text{m}$) with corresponding FWHMs (from top to bottom, right inset in (a), (b) and (c)).

The middle parts of Fig. 2 (a)-(c) is the optimal configuration of the metalens. The right parts show the simulation results of the corresponding ones, with the four wavelengths colored as red (1550 nm), yellow (1310 nm), green (1060 nm) and blue (910 nm) for vivid visualization, which shows the longitudinal intensity distributions and transvers patterns with full-width at half minimum (FWHM) from top to bottom. The corresponding values are shown in Table 1. One can see that the focal planes are in agreement with theoretical expectation, proving that we successfully control the chromatic aberration as expected. In theory, we can realize arbitrary chromatic aberration with this method by replacing the phase profiles with the target profiles. Here, we only demonstrate three typical instances as a proof of principle.

Table 1. The efficiency and FWHM of Metalens sample 1, 2, 3. The efficiency is defined as the ratio of the power of the spot at the focal plane to incident power.

| Wavelength (nm) | Metalens sample | Efficiency (%) | FWHM (μm) |
|-----------------|-----------------|----------------|------------------------|
| 910 | 1 | 29.5 | 1.052 |
| | 2 | 38.2 | 0.648 |
| | 3 | 40.2 | 0.665 |
| 1060 | 1 | 24.1 | 1.087 |
| | 2 | 34.6 | 0.687 |
| | 3 | 35.8 | 1.232 |
| 1310 | 1 | 42.7 | 1.289 |
| | 2 | 51.4 | 1.399 |
| | 3 | 45.1 | 0.826 |
| 1550 | 1 | 61.4 | 1.509 |
| | 2 | 46.7 | 1.646 |
| | 3 | 63.5 | 1.608 |

Note that the demonstration is only guaranteed for several discrete wavelengths, which is distinguished from previous reports on achromatic metalenses design within a continuous spectral bandwidth. [1–4,6,22,25,26]

3.2. Metalens-based color router

Wavelengths providing information in the spectral domain have been applied in material composition, temperature [27–29] and exoplanet search [30], which is recorded by the integration of a conventional Bayer-filter with CCD/CMOS [31]. The emergence of metalens-based color router (Meta-CR) is expected to overcome various aligned lithography steps for their manufacture with lower miniaturization, however, this geometric phase-based device requires circularly polarized light incident, which hinders its practical development [32].

Based on the discussion above, a polarization-independent Meta-CR has been proposed by our method, whose schematic diagram is depicted in Fig. 3(a). The required phase profile can be written as:

$$\varphi_{\text{MBCR}}(x, y, \lambda_i) = -\frac{2\pi}{\lambda_i}(\sqrt{(x + \Delta x)^2 + (y + \Delta y)^2 + f^2} - f) + \phi_{\text{shift}}(\lambda_i) \quad (6)$$

where Δx and Δy are offset distance of the focal position. In our design, the offset distance from the center of each spot is set as $2 \mu\text{m}$. Figure 3(b) gives the configuration of a $10 \mu\text{m} \times 10 \mu\text{m}$ polarization-independent Meta-CR and the simulation results are shown in Fig. 3(c) and (d), which can vividly show the situation when light containing the four wavelengths simultaneously incident. The efficiencies are 23.4% (910 nm), 28.9% (1060 nm), 28.0% (1310 nm) and 42.4% (1550 nm) for multiwavelength incident, respectively.

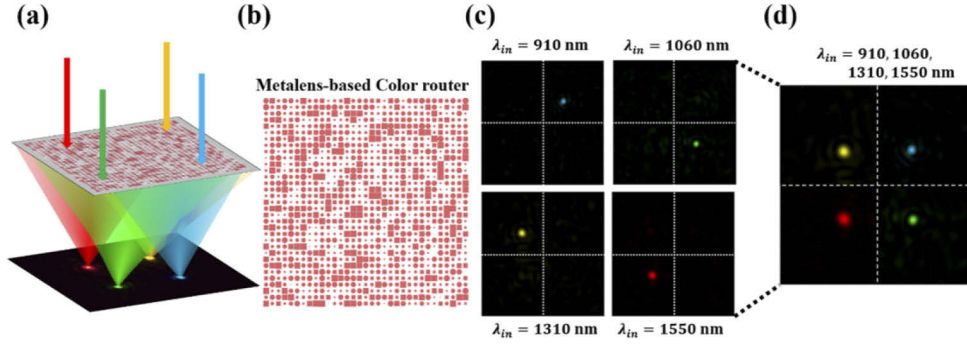


Fig. 3. (a). Schematic diagram of metalens-based color router. (b). Configuration of Meta-CR. (c), (d). Simulated transverse intensity distributions with four wavelengths incident simultaneously, scale bar: $2\mu\text{m}$.

3.3. Tri-functional structured light generator

Structured light plays a significant role in the fields of microscopy [33,34], communication [35] and astrophotonics [36]. How to achieve the multifunctional switching and take full advantage of a single-layer structured beam generator is the topic of our concern. For this reason, we select three wavelengths ($\lambda_1=910\text{ nm}$, $\lambda_2=1060\text{ nm}$ and $\lambda_3=1310\text{ nm}$) to complete this design.

For a proof-of-concept, a tri-functional metalens-based structured light generator (Fig. 4(a)) to generate focused orbital angular momentum (F-OAM) beam, Bessel beam and focused beam has been designed and numerically demonstrated. The phase profile must fulfill the following equations [16,37]:

$$\varphi_{\text{OAM}}(x, y) = -\frac{2\pi}{\lambda_1}(\sqrt{x^2 + y^2 + f^2} - f) + l\theta + \phi_{\text{shift}}^1(\lambda_1) \quad (7)$$

$$\varphi_{\text{Bessel}}(x, y) = -\frac{2\pi}{\lambda_2}(\sqrt{x^2 + y^2} \cdot \text{NA}) + \phi_{\text{shift}}^2(\lambda_2) \quad (8)$$

$$\varphi_{\text{focus}}(x, y) = -\frac{2\pi}{\lambda_3}(\sqrt{x^2 + y^2 + f^2} - f) + \phi_{\text{shift}}^3(\lambda_3) \quad (9)$$

where $\theta=\arctan(y/x)$ is the azimuthal angle, which represents the higher-order light imparted by the optical vortex, and l is the topological charge. NA is the numerical aperture of the metalens. Here, we set $l=1$ and $\text{NA}=0.6$. The tri-functional metalens samples produced by our optimal design method is illustrated in Fig. 4(b), and the simulation results with $\text{FWHM}_1^{\text{optimized}} \sim 0.736\ \mu\text{m}$, $\text{FWHM}_2^{\text{optimized}} \sim 0.600\ \mu\text{m}$, $\text{FWHM}_3^{\text{optimized}} \sim 1.348\ \mu\text{m}$ are shown in Fig. 4(c). While for the ideal situation displayed in Fig. 4(c), the corresponding results are $\text{FWHM}_1^{\text{ideal}} \sim 0.816\ \mu\text{m}$, $\text{FWHM}_2^{\text{ideal}} \sim 0.742\ \mu\text{m}$, $\text{FWHM}_3^{\text{ideal}} \sim 1.300\ \mu\text{m}$. Compared with the ideal results, the donut shape, Bessel pattern and focal spot are almost the same, FWHM differential of ideal and simulated results are merely $0.080\ \mu\text{m}$, $0.142\ \mu\text{m}$ and $0.048\ \mu\text{m}$, proving that the tri-structured light generator is of successfulness and robustness. One can see that the F-OAM beam has donut shape can be observed at $\lambda_1=910\text{ nm}$ incidence, while the generated Bessel beam at $\lambda_2=1060\text{ nm}$ propagates a long distance with a non-diffraction property, and a focused beam for $\lambda_3=1310\text{ nm}$ incidence coverages into a clear spot at the focal plane. The efficiencies for each beam are 28.7% , 43.0% and 36.0% , respectively, and the intensity distribution of the corresponding light fields with less crosstalk can be apparently seen in Fig. 4(c).

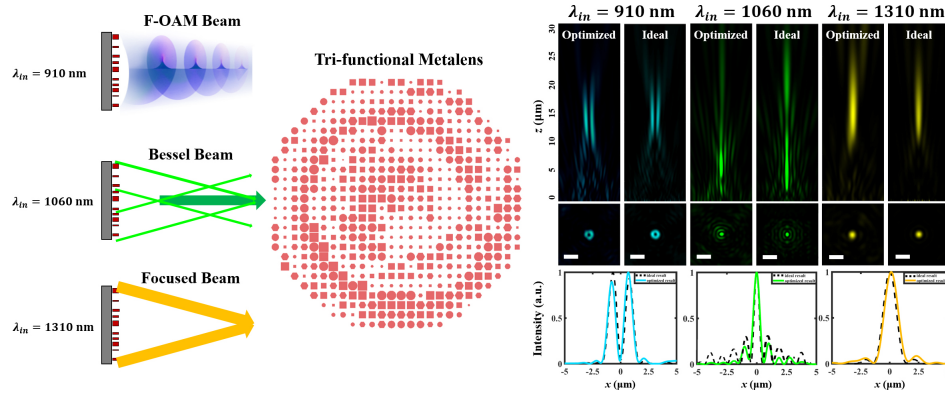


Fig. 4. (a). Schematic diagram of tri-functional metalens-based structured light generator. (b). Configuration of metalens. (c). Comparison of simulated longitudinal intensity distributions, transverse intensity distributions of ideal and optimized results with corresponding FWHMs (from top to bottom). Solid lines represent optimized results; dash lines denote as ideal results. Scale bar: $2\mu\text{m}$.

4. Conclusion

In summary, we employ the genetic algorithm optimization to arbitrarily manipulate the chromatic dispersion based on metalenses, and then we design the metalens-based color router in the near infrared region. Finally, we show the multifunctional structured light generator that can modulate more complex phase profiles at different wavelengths. Additionally, the meta-devices in this work possess a polarization-independent property due to the phase library consisting of centrosymmetric nanopillars. Metalens based on the optimization algorithm can not only allow multiple functions by utilizing the dimension of wavelength, but also have the merits of miniaturization and integration, which are expected to apply in the next generation of optical platform. We also anticipate that wavelength-multiplexing multifunctional metalenses have greater potential in computer science.

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Data availability. Data underlying the results presented in this paper are not publicly available at this time but may be obtained from the authors upon reasonable request.

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